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**AUSTRALIAN ATOMIC ENERGY COMMISSION  
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LUCAS HEIGHTS RESEARCH LABORATORIES**

**SPECACT, A FORTRAN PROGRAM FOR THE  
ROUTINE CALCULATION OF THE SPECIFIC ACTIVITY OF  
FISSION-PRODUCED MOLYBDENUM-99**

by

**R.K. BARNES  
E.L.R. HETHERINGTON**

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ABSTRACT

The specific activity of  $^{99}\text{Mo}$  is an important factor in the production of  $^{99}\text{Mo}/^{99m}\text{Tc}$  generators, used in nuclear medicine. Molybdenum-99 formed *via* the fission route is not carrier free but is contaminated by a number of stable molybdenum isotopes formed concurrently during neutron irradiation of the uranium target. The specific activity of fission-based  $^{99}\text{Mo}$  is therefore a function of irradiation time and post-irradiation decay. A computer program, written in FORTRAN, is presented for defining routinely the specific activity of fission-based  $^{99}\text{Mo}$ .

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FORTRAN; S CODES; MOLYBDENUM 99; RADIOACTIVITY; NUCLEAR DECAY; IRRADIATION;  
MASS; NEUTRON FLUX; URANIUM 235 TARGET; FISSION YIELD

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## 1. INTRODUCTION

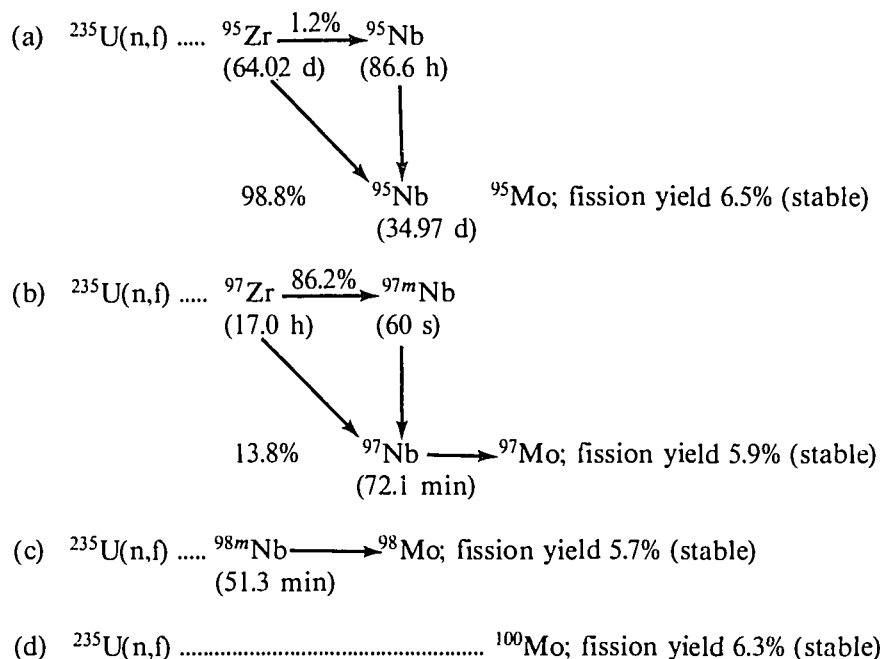
Since 1970,  $^{99m}\text{Tc}$  generators based upon fission-produced  $^{99}\text{Mo}$  have gained a greater acceptability in nuclear medicine than those from  $(n,\gamma)$  derived  $^{99}\text{Mo}$ . This increase in popularity may be attributed partly to the very high specific activities of  $^{99}\text{Mo}$  attainable using the fission pathway.

Technetium-99m generators prepared from fission-based  $^{99}\text{Mo}$  having very high specific activities have demonstrated significantly improved elution characteristics when compared with generators prepared from low specific activity  $^{99}\text{Mo}$ , produced from  $(n,\gamma)$  reactions [Boyd 1973]. Additionally, in the production of high activity  $^{99m}\text{Tc}$  generators it is important to ensure that the maximum sorption capacity of the alumina bed employed in the generator is not approached, as this may lead to high  $^{99}\text{Mo}$  breakthrough during the elution cycle of the generator and therefore compromise the radionuclidic purity of acquired  $^{99m}\text{Tc}$ . Hence a knowledge of the specific activity of  $^{99}\text{Mo}$  is an important factor in the preparation of  $^{99}\text{Mo}/^{99m}\text{Tc}$  generators for use in nuclear medicine.

The computer program SPECFACT was developed, as a part of the quality control regime, for assessing routinely the specific activity of fission-produced  $^{99}\text{Mo}$ , prepared at Lucas Heights. This program computes the specific activity of  $^{99}\text{Mo}$  based upon neutron-irradiation and post-irradiation decay parameters of the uranium target.

## 2. SPECIFIC ACTIVITY OF FISSION PRODUCED MOLYBDENUM-99

Molybdenum-99 is formed directly from  $^{235}\text{U}$  and has a cumulative fission yield of 6.1 per cent [Rose and Burrows 1976] in a flux of thermal neutrons; however, when formed by this pathway it is not 'carrier free' but contains a number of stable molybdenum isotopes which are formed concurrently, during the irradiation process, by the following reactions:



In addition to being formed directly in the fission process,  $^{99}\text{Mo}$  is also produced by neutron activation of the stable  $^{98}\text{Mo}$  formed in reaction (c); however, it was computed that the activity of  $^{99}\text{Mo}$  derived from this source is less than one per cent of the total  $^{99}\text{Mo}$  activity. Short-lived fission-produced molybdenum, such as  $^{102}\text{Mo}$ - $^{107}\text{Mo}$  with half-lives of less than 12 minutes, makes insignificant contributions to the specific activity of  $^{99}\text{Mo}$  and was therefore not considered in the program. Reactions (a) to (d) effectively reduce the specific activity from its carrier-free value of  $4.79 \times 10^5 \text{ Ci g}^{-1} \text{}^{99}\text{Mo}$  by factors of up to 20, depending on the level of irradiation and the decay times.

### 3. METHOD OF CALCULATION

#### 3.1 Activation Equations

During the neutron irradiation of a uranium target, the build-up of fission fragments in a fission chain of the type  $^{235}\text{U}(n,f) \cdots N_1 \longrightarrow N_2 \longrightarrow N_3$  in which  $N_1$ ,  $N_2$  and  $N_3$  are radioactive fission fragments, is given by the general activation equations (refer to section 7 for definition of notation):

$$N_1 = \frac{K_1}{\lambda_1} (1 - e^{-\lambda_1 t})$$

$$N_2 = \frac{K_1 + K_2}{\lambda_2} (1 - e^{-\lambda_2 t}) - \frac{K_1}{(\lambda_2 - \lambda_1)} (e^{-\lambda_1 t} - e^{-\lambda_2 t})$$

$$N_3 = \frac{K_1 + K_2 + K_3}{\lambda_3} (1 - e^{-\lambda_3 t}) - \frac{(K_1 + K_2)}{(\lambda_3 - \lambda_2)} (e^{-\lambda_2 t} - e^{-\lambda_3 t})$$

$$- K_1 \lambda_2 \left\{ \frac{e^{-\lambda_1 t}}{(\lambda_2 - \lambda_1)(\lambda_3 - \lambda_1)} + \frac{e^{-\lambda_2 t}}{(\lambda_1 - \lambda_2)(\lambda_3 - \lambda_2)} \right.$$

$$\left. + \frac{e^{-\lambda_3 t}}{(\lambda_1 - \lambda_3)(\lambda_2 - \lambda_3)} \right\}$$

The production of the niobium intermediates in reactions (a) and (b), arise almost solely from direct decay of the respective zirconium precursors. The direct fission yield of these intermediates is so low that the values of  $K_2$  and  $K_3$ , in the activation equation (B) and (C), can be considered to be zero.

The application of equations (A), (B) and (C) assumes that  $N_\mu$  remains essentially constant throughout the irradiation period. For short irradiation periods of less than ten days, as is used at Lucas Heights, and at neutron fluxes of between  $8 \times 10^{13}$  to  $1.0 \times 10^{14}$  n cm<sup>-2</sup> s<sup>-1</sup>, there is little target burn-up and the value of  $N_\mu$  remains essentially constant throughout the period of irradiation.

#### 3.2 Post-irradiation Decay Equations

During the post-irradiation phase, stable molybdenum nuclides are still being generated from decay of the parent and daughter fission fragments, as indicated in reactions (a), (b) and (c). The decay of these fragments has the effect of reducing the specific activity of <sup>99</sup>Mo.

The amount of the radioactive species,  $N_1$ ,  $N_2$  and  $N_3$  remaining after time  $T$  in a multiple step decay chain is given by  $N_1 = N_1^0 e^{-\lambda_1 T}$

$$N_2 = \frac{N_1^0 \lambda_1}{\lambda_2 - \lambda_1} (e^{-\lambda_1 T} - e^{-\lambda_2 T}) + N_2^0 e^{-\lambda_2 T}$$

$$N_3 = N_3^0 e^{-\lambda_3 T} + N_2^0 \frac{\lambda_2}{\lambda_3 - \lambda_2} (e^{-\lambda_2 T} - e^{-\lambda_3 T})$$

$$+ N_1^0 \left\{ \frac{\lambda_1}{(\lambda_2 - \lambda_1)(\lambda_3 - \lambda_1)} \frac{\lambda_2}{\lambda_3 - \lambda_1} e^{-\lambda_1 T} + \frac{\lambda_1}{(\lambda_1 - \lambda_2)(\lambda_3 - \lambda_2)} \frac{\lambda_2}{\lambda_3 - \lambda_2} e^{-\lambda_2 T} \right.$$

$$\left. + \frac{\lambda_1}{(\lambda_1 - \lambda_3)(\lambda_2 - \lambda_3)} \frac{\lambda_2}{\lambda_2 - \lambda_3} e^{-\lambda_3 T} \right\}$$

In this case  $T$  is the time lapse between reactor discharge and generator loading.

### 4. PROGRAM

The program computes the activity of <sup>99</sup>Mo and the total mass of each of the molybdenum isotopes formed during neutron irradiation, taking into account the branching ratios in reactions (a) and (b). Similarly, during the post-irradiation phase, the specific activity of <sup>99</sup>Mo is affected by the decay of <sup>99</sup>Mo and the ingrowth of stable molybdenum species from the parent-daughter fission fragments.

The input parameters for the program include the neutron flux and irradiation time followed by the post-irradiation decay time (Appendix A). The computer output gives the individual masses for each of the molybdenum isotopes produced, in addition to the total activity and specific activity for  $^{99}\text{Mo}$  (see Appendix B for typical output).

## 5. CONCLUSIONS

The program SPECACT was written to monitor routinely the specific activity of fission-based  $^{99}\text{Mo}$  produced at Lucas Heights as part of its quality assurance regime for the preparation of  $^{99}\text{Mo}/^{99m}\text{Tc}$  generators. The program input simply requires the values of neutron flux, irradiation time and post-irradiation decay time to be entered to complete the specific activity calculations.

## 6. REFERENCES

- Boyd, R. [1973] - In *Radiopharmaceuticals and Labelled Compounds*, Vol.1, p.3. IAEA, Vienna.  
 Rose, P.F., Burrows, T.W. [1976] - *Fission Product Decay Data*, Vol.1, BNL-NCS-50545.

## 7. NOTATION

$K_1$	=	$Y_1 \sigma_f \phi N_\mu$
$K_2$	=	$Y_2 \sigma_f \phi N_\mu$
$K_3$	=	$Y_3 \sigma_f \phi N_\mu$
$t$	=	time of irradiation.
$T$	=	post-irradiation decay time.
$\lambda_1$	=	decay constant of the parent fission fragment with $N_1$ atoms at time $t$ .
$\lambda_2$	=	decay constant of the fission product with $N_2$ atoms at time $t$ .
$\lambda_3$	=	decay constant of the fission product with $N_3$ atoms at time $t$ .
$\sigma_f$	=	fission cross section of uranium (580 barns for $^{235}\text{U}$ ).
$N_\mu$	=	number of atoms of uranium in target.
$N_1^0$	=	amount of species $N_1$ at $T = 0$ .
$N_2^0$	=	amount of species $N_2$ at $T = 0$ .
$N_3^0$	=	amount of species $N_3$ at $T = 0$ .
$\phi$	=	neutron flux.
$Y_1$	}	= the fission yields of $N_1$ , $N_2$ and $N_3$ respectively.
$Y_2$		
$Y_3$		

APPENDIX A  
LISTING OF THE PROGRAM SPECACT

```

IMPLICIT REAL (K-N)
DOUBLE PRECISION DT,TC,DI,TI,L1,L2,L3,L4,L5,L6,L7,L8
NU=6.0248E23/235.
SIG=560.*1.0E-24
FLUX=1.0E14
L1=.693147/(64.02*8.64D4)
L2=.693147/(86.6*3.6D3)
L3=.693147/(34.97*8.64D4)
L4=.693147/(17.0*3.6D3)
L5=.693147/60.0
L6=.693147/(72.1*60.)
L7=.693147/(51.3*60.)
L8=.693147/(66.02*3.6D3)
Y1=0.0646
Y2=0.0595
Y3=0.0573
Y4=0.0610
Y5=0.0630
K1=Y1*NU*SIG*FLUX
K2=Y2*NU*SIG*FLUX
K3=Y3*NU*SIG*FLUX
K4=Y4*NU*SIG*FLUX
DI=0.0
DO 99 J=1,21
DI=DI+1.0
IF(MOD(J,2).EQ.0) WRITE(3,3)
IF(MOD(J,2).NE.0) WRITE(3,6)
6 FORMAT('1 ')
3 FORMAT(/////)
WRITE(3,1)DI
1 FORMAT(' IRRADIATION TIME = ',F4.1,' DAYS')
TI=DI*8.64D4
TC=-1.0
WRITE(3,2)
WRITE(3,8)
WRITE(3,9)
2 FORMAT(' DECAY ACTIVITY MASS MASS MASS
1 MASS MASS MASS SPECIFIC')
8 FORMAT(' TIME M099 M095 M097 M098
1 M099 M0100 MOLYBDENUM ACTIVITY')
9 FORMAT(' DAYS CURIE GRAM GRAM GRAM
1 GRAM GRAM GRAM CURIE/GRAM')
DO 88 JJ=1,21
TC=TC+1.
DT=TC*8.64D4
ATM5=K1*TI
N1=K1/L1*(1.0-DEXP(-L1*TI))
N2=K1/L2*(1.-DEXP(-L2*TI))-K1/(L2-L1)*(DEXP(-L1*TI)-DEXP(-L2*TI))
N2=N2*0.012
N3=K1/L3*(1.-DEXP(-L3*TI))-K1/(L3-L2)*(DEXP(-L2*TI)-DEXP(-L3*TI))
A=DEXP(-L1*TI)/(L2-L1)/(L3-L1)
B=DEXP(-L2*TI)/(L1-L2)/(L3-L2)
C=DEXP(-L3*TI)/(L1-L3)/(L2-L3)

```



```

N5=N5-K1*L2*(A+B+C)
N3=N3*0.012
N3B=K1/L3*(1.-DEXP(-L3*TI))-K1/(L3-L1)*(DEXP(-L1*TI)-DEXP(-L3*TI))
N3B=N3B*0.933
N3=N3+N3B
NN1=N1*DEXP(-L1*DT)
NN2=0.012*L1*N1/(L2-L1)*(DEXP(-L1*DT)-DEXP(-L2*DT))+N2*DEXP(-L2*DT
1)
P=L1*L2*DEXP(-L1*DT)/(L2-L1)/(L3-L1)
Q=L1*L2*DEXP(-L2*DT)/(L1-L2)/(L3-L2)
R=L1*L2*DEXP(-L3*DT)/(L1-L3)/(L2-L3)
S=N2*L2/(L3-L2)*(DEXP(-L2*DT)-DEXP(-L3*DT))
T=0.788*L1*N1/(L3-L1)*(DEXP(-L1*DT)-DEXP(-L3*DT))+N3*DEXP(-L3*DT)
NN3=S+0.012*N1*(P+Q+R)+T
M095=ATM5-(NN1+NN2+NN3)
MAS5=95./6.0248E23*M095
ATM7=K2*TI
N4=K2/L4*(1.-DEXP(-L4*TI))
N5=K2/L5*(1.-DEXP(-L5*TI))-K2/(L5-L4)*(DEXP(-L4*TI)-DEXP(-L5*TI))
N5=N5*0.862
N6=K2/L6*(1.-DEXP(-L6*TI))-K2/(L6-L5)*(DEXP(-L5*TI)-DEXP(-L6*TI))
D=DEXP(-L4*TI)/(L5-L4)/(L6-L4)
E=DEXP(-L5*TI)/(L4-L5)/(L6-L5)
F=DEXP(-L6*TI)/(L4-L6)/(L5-L6)
N6=N6-K2*L5*(D+E+F)
N6=0.862*N6
N6B=K2/L6*(1.-DEXP(-L6*TI))-K2/(L6-L4)*(DEXP(-L4*TI)-DEXP(-L6*TI))
N6B=N6B*0.138
N6=N6+N6B
NN4=N4*DEXP(-L4*DT)
NN5=0.862*L4*N4/(L5-L4)*(DEXP(-L4*DT)-DEXP(-L5*DT))+N5*DEXP(-L5*DT
1)
P1=L4*L5*DEXP(-L4*DT)/(L5-L4)/(L6-L4)
Q1=L4*L5*DEXP(-L5*DT)/(L4-L5)/(L6-L5)
R1=L4*L5*DEXP(-L6*DT)/(L4-L6)/(L5-L6)
S1=N5*L5/(L6-L5)*(DEXP(-L5*DT)-DEXP(-L6*DT))
T1=0.138*L4*N4/(L6-L4)*(DEXP(-L4*DT)-DEXP(-L6*DT))+N6*DEXP(-L6*DT)
NN6=S1+0.862*N4*(P1+Q1+R1)+T1
M097=ATM7-(NN4+NN5+NN6)
MAS7=97./6.0248E23*M097
ATM8=K3*TI
N7=K3/L7*(1.-DEXP(-L7*TI))
NN7=N7*DEXP(-L7*DT)
7 M098=ATM8-NN7
MAS8=98./6.0248E23*M098
N8=K4/L8*(1.-DEXP(-L8*TI))
NN8=N8*DEXP(-L8*DT)
ACT9=NN8*L8/3.7E10
MAS9=99./6.0248E23*NN8
ATM1=Y5*NU*SIG*FLUX*TI
MAS1=100./6.0248E23*ATM1
MAS5=MAS5+MAS7+MAS8+MAS9+MAS1
SACT=ACT9/MAS5
WRITE(3,4)TC,ACT9,MAS5,MAS7,MAS8,MAS9,MAS1,MAS5,SACT
4 FORMAT(F6.1,F12.3,1P7E12.3)
88 CONTINUE
99 CONTINUE
STOP
END

```

APPENDIX B  
TYPICAL OUTPUT

IRRADIATION TIME = 7.0 DAYS								
DECAY TIME DAYS	ACTIVITY CURIE	MASS MO99 GRAM	MASS MO97 GRAM	MASS MO98 GRAM	MASS MO99 GRAM	MASS MO100 GRAM	MASS MOLYBDENUM GRAM	SPECIFIC ACTIVITY CURIE/GRAM
0.0	203.134	1.509E-06	7.269E-04	8.321E-04	4.235E-04	9.404E-04	2.924E-03	6.946E+04
1.0	157.888	2.232E-06	8.107E-04	8.382E-04	3.292E-04	9.404E-04	2.921E-03	5.406E+04
2.0	122.721	3.125E-06	8.424E-04	8.382E-04	2.558E-04	9.404E-04	2.880E-03	4.261E+04
3.0	95.386	4.182E-06	8.543E-04	8.382E-04	1.989E-04	9.404E-04	2.836E-03	3.303E+04
4.0	74.140	5.401E-06	8.588E-04	8.382E-04	1.546E-04	9.404E-04	2.797E-03	2.650E+04
5.0	57.626	6.774E-06	8.605E-04	8.382E-04	1.201E-04	9.404E-04	2.766E-03	2.083E+04
6.0	44.791	8.297E-06	8.611E-04	8.382E-04	9.338E-05	9.404E-04	2.741E-03	1.634E+04
7.0	34.814	9.966E-06	8.614E-04	8.382E-04	7.258E-05	9.404E-04	2.723E-03	1.279E+04
8.0	27.060	1.178E-05	8.615E-04	8.382E-04	5.641E-05	9.404E-04	2.708E-03	9.972E+03
9.0	21.033	1.372E-05	8.615E-04	8.382E-04	4.385E-05	9.404E-04	2.698E-03	7.797E+03
10.0	16.348	1.580E-05	8.615E-04	8.382E-04	3.408E-05	9.404E-04	2.690E-03	6.077E+03
11.0	12.707	1.800E-05	8.615E-04	8.382E-04	2.649E-05	9.404E-04	2.685E-03	4.735E+03
12.0	9.876	2.033E-05	8.615E-04	8.382E-04	2.059E-05	9.404E-04	2.681E-03	3.634E+03
13.0	7.676	2.278E-05	8.615E-04	8.382E-04	1.600E-05	9.404E-04	2.679E-03	2.866E+03
14.0	5.967	2.534E-05	8.615E-04	8.382E-04	1.244E-05	9.404E-04	2.678E-03	2.228E+03
15.0	4.638	2.801E-05	8.615E-04	8.382E-04	9.668E-06	9.404E-04	2.678E-03	1.732E+03
16.0	3.605	3.079E-05	8.615E-04	8.382E-04	7.515E-06	9.404E-04	2.678E-03	1.340E+03
17.0	2.802	3.368E-05	8.615E-04	8.382E-04	5.841E-06	9.404E-04	2.680E-03	1.046E+03
18.0	2.178	3.666E-05	8.615E-04	8.382E-04	4.540E-06	9.404E-04	2.681E-03	8.122E+02
19.0	1.693	3.974E-05	8.615E-04	8.382E-04	3.529E-06	9.404E-04	2.683E-03	6.303E+02
20.0	1.315	4.291E-05	8.615E-04	8.382E-04	2.743E-06	9.404E-04	2.686E-03	4.899E+02

IRRADIATION TIME = 8.0 DAYS								
DECAY TIME DAYS	ACTIVITY CURIE	MASS MO99 GRAM	MASS MO97 GRAM	MASS MO98 GRAM	MASS MO99 GRAM	MASS MO100 GRAM	MASS MOLYBDENUM GRAM	SPECIFIC ACTIVITY CURIE/GRAM
0.0	212.492	2.236E-06	8.499E-04	9.518E-04	4.430E-04	1.075E-03	3.322E-03	6.397E+04
1.0	165.162	3.156E-06	9.337E-04	9.530E-04	3.443E-04	1.075E-03	3.314E-03	4.984E+04
2.0	128.374	4.268E-06	9.655E-04	9.530E-04	2.676E-04	1.075E-03	3.270E-03	3.926E+04
3.0	99.731	5.566E-06	9.774E-04	9.530E-04	2.030E-04	1.075E-03	3.224E-03	3.095E+04
4.0	77.556	7.044E-06	9.819E-04	9.530E-04	1.617E-04	1.075E-03	3.183E-03	2.436E+04
5.0	60.281	8.676E-06	9.836E-04	9.530E-04	1.257E-04	1.075E-03	3.151E-03	1.913E+04
6.0	46.854	1.052E-05	9.842E-04	9.530E-04	9.768E-05	1.075E-03	3.125E-03	1.499E+04
7.0	36.413	1.250E-05	9.844E-04	9.530E-04	7.592E-05	1.075E-03	3.106E-03	1.173E+04
8.0	28.306	1.445E-05	9.845E-04	9.530E-04	5.901E-05	1.075E-03	3.091E-03	9.158E+03
9.0	22.002	1.694E-05	9.846E-04	9.530E-04	4.537E-05	1.075E-03	3.080E-03	7.143E+03
10.0	17.101	1.939E-05	9.846E-04	9.530E-04	3.565E-05	1.075E-03	3.072E-03	5.566E+03
11.0	13.297	2.193E-05	9.846E-04	9.530E-04	2.771E-05	1.075E-03	3.067E-03	4.334E+03
12.0	10.331	2.470E-05	9.846E-04	9.530E-04	2.134E-05	1.075E-03	3.064E-03	3.372E+03
13.0	8.030	2.756E-05	9.846E-04	9.530E-04	1.674E-05	1.075E-03	3.062E-03	2.623E+03
14.0	6.242	3.055E-05	9.846E-04	9.530E-04	1.301E-05	1.075E-03	3.061E-03	2.039E+03
15.0	4.851	3.366E-05	9.846E-04	9.530E-04	1.011E-05	1.075E-03	3.061E-03	1.585E+03
16.0	3.771	3.690E-05	9.846E-04	9.530E-04	7.861E-06	1.075E-03	3.062E-03	1.231E+03
17.0	2.931	4.025E-05	9.846E-04	9.530E-04	6.110E-06	1.075E-03	3.064E-03	9.567E+02
18.0	2.278	4.371E-05	9.846E-04	9.530E-04	4.749E-06	1.075E-03	3.066E-03	7.431E+02
19.0	1.771	4.728E-05	9.846E-04	9.530E-04	3.691E-06	1.075E-03	3.068E-03	5.771E+02
20.0	1.376	5.095E-05	9.846E-04	9.530E-04	2.869E-06	1.075E-03	3.071E-03	4.481E+02